

Thurs: HW by 5pm

Fri: ZOOM

Consistency of the field equations

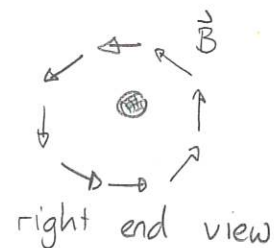
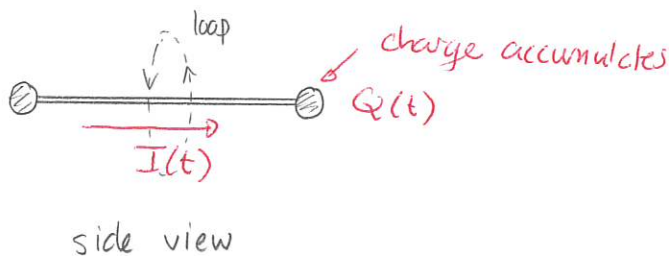
So far we have as field equations:

$$\begin{aligned} \vec{\nabla} \cdot \vec{E} &= \rho / \epsilon_0 \\ \vec{\nabla} \times \vec{E} &= -\frac{\partial \vec{B}}{\partial t} \\ \vec{\nabla} \cdot \vec{B} &= 0 \\ \vec{\nabla} \times \vec{B} &= \mu_0 \vec{J} \end{aligned}$$

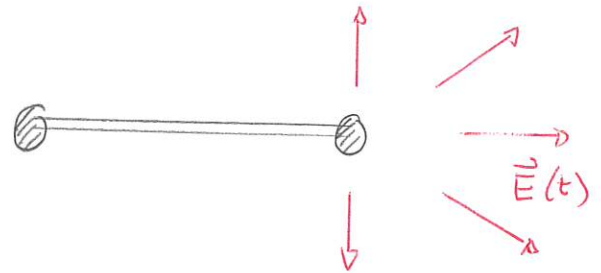
with the current and charge densities required to satisfy the continuity equation:

$$\vec{\nabla} \cdot \vec{J} + \frac{\partial \rho}{\partial t} = 0$$

We will see that these are not consistent both mathematically and physically. First consider a physical situation of a current along a finite straight segment



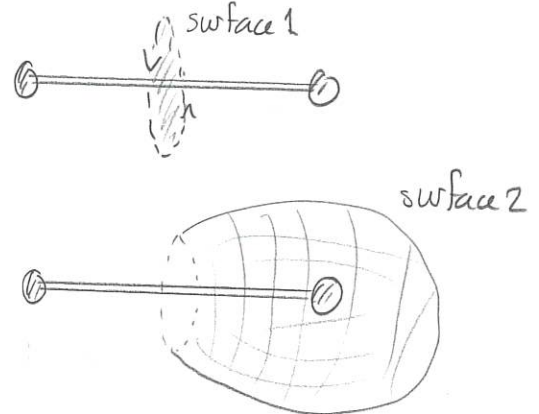
The Biot-Savart law predicts that the current will produce a magnetic field that circles the wire. Separately Coulomb's law predicts that the point charges at the ends produce a time-varying electric field, which will have a structure similar to an electric dipole field.



Now consider a line integral along a circular loop in a plane perpendicular to the wire. Mathematically

$$\oint_{\text{loop}} \vec{B} \cdot d\vec{l} = \int_{\text{surface}} \vec{\nabla} \times \vec{B} \cdot d\vec{a}$$

$$= \mu_0 \int_{\text{surface}} \vec{J} \cdot d\vec{a}$$



where the surface is any surface with the loop as its boundary. Thus we get

$$\int_{\text{surface 1}} \vec{J} \cdot d\vec{a} \neq 0 \quad \text{and} \quad \int_{\text{surface 2}} \vec{J} \cdot d\vec{a} = 0$$

Depending on which surface we use we get

$$\oint \vec{B} \cdot d\vec{l} \neq 0 \quad (\text{surface 1})$$

$$\oint \vec{B} \cdot d\vec{l} = 0 \quad (\text{surface 2})$$

But the magnetic fields cannot depend on the surface and the rule $\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$ cannot be correct in this case.

When could this rule be correct? An alternative piece of mathematics is that, for any vector field $\vec{\nabla} \cdot (\vec{\nabla} \times \vec{A}) = 0$. Then we check this for electric and magnetic fields:

Electric	Magnetic
$\vec{\nabla} \cdot (\vec{\nabla} \times \vec{E}) = \vec{\nabla} \cdot \left(-\frac{\partial \vec{B}}{\partial t} \right)$ $= -\frac{\partial}{\partial t} (\vec{\nabla} \cdot \vec{B})$ $\stackrel{ }{=} 0$ $= 0$	$\vec{\nabla} \cdot (\vec{\nabla} \times \vec{B}) = \mu_0 (\vec{\nabla} \cdot \vec{J})$ $\stackrel{ }{=} 0$ $\Rightarrow \vec{\nabla} \cdot \vec{J} = 0 \quad \Rightarrow \frac{\partial \rho}{\partial t} = 0$

Thus the field equations so far are only correct when $\vec{\nabla} \cdot \vec{J} = 0$ and $\frac{\partial \rho}{\partial t} = 0$.

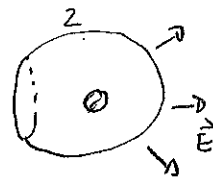
This is the electrostatic case. So

$\vec{\nabla} \cdot \vec{E} = \rho / \epsilon_0$	$\vec{\nabla} \cdot \vec{B} = 0$	are only true if $\frac{\partial \rho}{\partial t} = 0$ and $\vec{\nabla} \cdot \vec{J} = 0$
$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$	$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J}$	

These are clearly not the case for the finite wire example. How could they be modified? We note that if $\frac{\partial \vec{E}}{\partial t}$ contributed as a source to the magnetic field then this would add to the integrals

$$\int \vec{\nabla} \times \vec{B} \cdot d\vec{a}$$

and thus we may get non-zero for the integral over the second surface.



Magnetic field induction

Suppose that there is an additional source of magnetic field \vec{Z} .

Then:

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J} + \vec{Z}$$

Now

$$\underbrace{\vec{\nabla} \cdot (\vec{\nabla} \times \vec{B})}_0 = \mu_0 \underbrace{\vec{\nabla} \cdot \vec{J}}_{-\frac{\partial \rho}{\partial t}} + \vec{\nabla} \cdot \vec{Z}$$

$$\begin{aligned} \Rightarrow \vec{\nabla} \cdot \vec{Z} &= \mu_0 \frac{\partial \rho}{\partial t} \\ &= \mu_0 \frac{\partial}{\partial t} \epsilon_0 \vec{\nabla} \cdot \vec{E} \end{aligned}$$

$$\Rightarrow \vec{\nabla} \cdot \vec{Z} = \vec{\nabla} \cdot \left[\mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t} \right]$$

So one possible solution is $\vec{Z} = \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$. Then:

$$\boxed{\begin{aligned} \vec{\nabla} \times \vec{B} &= \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t} \\ \vec{\nabla} \cdot \vec{B} &= 0 \end{aligned}}$$

are the equations for magnetic fields. We see that a time-varying electric field can induce a magnetic field. In the case where $\vec{J} = 0$

$$\begin{aligned} \vec{\nabla} \cdot \vec{B} &= 0 \\ \vec{\nabla} \times \vec{B} &= \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t} \end{aligned}$$

which means fields can be determined in the usual way by replacing

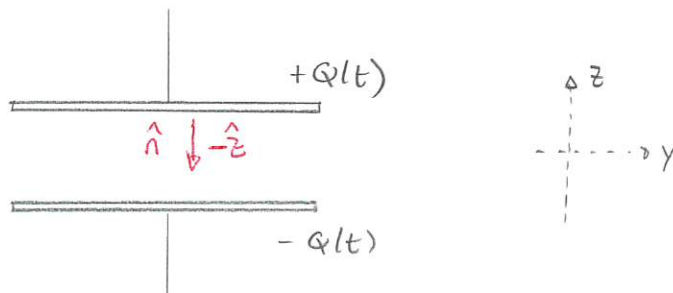
$$\vec{J} \rightarrow \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

1 Fields between two capacitor plates

A parallel plate capacitor has circular plates with radius R and are separated by a small enough distance to regard as infinite. The plates are connected to a source that charges them with opposite charges and the charge on one plate is $Q(t)$. Assume that this is uniformly distributed on the plate and varies relatively slowly.

- Determine an expression for the electric field produced between the plates by the charges on the plates.
- Determine the magnetic field produced by the time-varying electric field at any location on a plane midway between the plates.

Answer: a)



Between a pair of parallel plates,

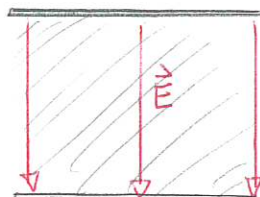
$$\vec{E} = \frac{\sigma}{\epsilon_0} \hat{n} = \frac{Q(t)/A}{\epsilon_0} (-\hat{z}) \quad A = \pi R^2$$

$$\Rightarrow \vec{E} = - \frac{Q(t)}{\epsilon_0 \pi R^2} \hat{z}$$

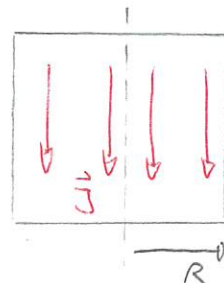
$$b) \quad \vec{\nabla} \times \vec{B} = \underbrace{\mu_0 \vec{j}}_0 + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t} \quad \Rightarrow \quad \vec{\nabla} \times \vec{B} = \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

between plates

Then, inside the plates \vec{E} is uniform. This is analogous to a source current density



$$\vec{E} = 0$$



We will use an analog of Ampère's Law to evaluate \vec{B} . First

$$\vec{B} = B_s \hat{s} + B_\phi \hat{\phi} + B_z \hat{z}$$

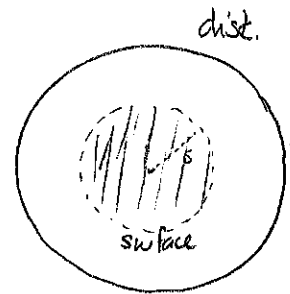
By the Biot-Savart type argument, $B_z = 0$. By a symmetry argument $B_s = 0$.

Thus

$$\vec{B} = B_\phi(s) \hat{\phi} \quad (\text{only along midplane!})$$

We can integrate along a circular loop of radius s . Then

$$\begin{aligned} \oint_{\text{loop}} \vec{B} \cdot d\vec{l} &= \int_{\text{surface}} \vec{\nabla} \times \vec{B} \cdot d\vec{a} \\ &= \mu_0 \epsilon_0 \int_{\text{surface}} \frac{\partial \vec{E}}{\partial t} \cdot d\vec{a} \end{aligned}$$



For the l.h.s.

$$\left. \begin{array}{l} s' = s \\ 0 < \phi' < 2\pi \\ z' = 0 \end{array} \right\} d\vec{l} = s' d\phi' \hat{\phi} = s d\phi' \hat{\phi}$$

$$\Rightarrow \oint_{\text{loop}} \vec{B} \cdot d\vec{l} = \int_0^{2\pi} B_\phi(s) s d\phi' = 2\pi s B_\phi(s)$$

Thus

$$2\pi s B_\phi(s) = \mu_0 \epsilon_0 \int \frac{\partial \vec{E}}{\partial t} \cdot d\vec{a}$$

$$\Rightarrow B_\phi(s) = \frac{\mu_0 \epsilon_0}{2\pi s} \int \frac{\partial \vec{E}}{\partial t} \cdot d\vec{a}$$

Case 1 $s \leq R$. The l.h.s requires

$$\left. \begin{array}{l} 0 < s' \leq s \\ 0 \leq \phi' \leq 2\pi \\ z' = 0 \end{array} \right\} d\vec{a} = s' ds' d\phi' \hat{z}$$

$$B_{\phi}(s) = - \frac{\mu_0 \epsilon_0}{2\pi s} \int_0^s ds' \int_0^{2\pi} d\phi' s' \frac{dQ}{dt} \frac{1}{\epsilon_0 \pi R^2}$$

$$= - \frac{\mu_0}{2\pi s} \frac{dQ}{dt} \frac{s^2}{R^2} \quad \Rightarrow \quad B_{\phi}(s) = - \frac{\mu_0 s}{2\pi R^2} \frac{dQ}{dt}$$

Case 2 $s \geq R$ The only difference is $0 < s' \leq R$. This gives

$$B_{\phi}(s) = - \frac{\mu_0}{2\pi s} \frac{dQ}{dt}$$

Thus we get

$$\vec{B} = \begin{cases} - \frac{\mu_0 s}{2\pi R^2} \frac{dQ}{dt} \hat{\phi} & s \leq R \\ - \frac{\mu_0}{2\pi s} \frac{dQ}{dt} \hat{\phi} & s \geq R \end{cases}$$

We could attempt to check $\vec{\nabla} \cdot \vec{B} = 0$ and $\vec{\nabla} \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$ in the region between the plates. We know $B_z = 0$ and also none of the fields depends on ϕ . Then:

$$\begin{aligned} \vec{\nabla} \cdot \vec{B} &= \frac{1}{s} \frac{\partial}{\partial s} (s B_s) + \frac{1}{s} \frac{\partial B_{\phi}}{\partial \phi} + \frac{\partial B_z}{\partial z} \\ &= \frac{1}{s} \frac{\partial}{\partial s} (s B_s) \end{aligned}$$

In the midplane $B_s = 0$ and thus $\vec{\nabla} \cdot \vec{B} = 0$.

Now

$$\begin{aligned}\vec{\nabla} \times \vec{B} &= \left[\frac{1}{s} \frac{\partial B_z}{\partial \phi} - \frac{\partial B_\phi}{\partial z} \right] \hat{s} + \left[\frac{\partial B_s}{\partial z} - \frac{\partial B_z}{\partial s} \right] \hat{\phi} + \frac{1}{s} \left[\frac{\partial}{\partial s} (s B_\phi) - \frac{\partial B_s}{\partial \phi} \right] \hat{z} \\ &= - \frac{\partial B_\phi}{\partial z} \hat{s} + \frac{\partial B_s}{\partial z} \hat{\phi} + \frac{1}{s} \frac{\partial}{\partial s} (s B_\phi) \hat{z}\end{aligned}$$

By typical Biot-Savart type arguments $B_s = 0$. However, we do not have a notion of how B_ϕ varies with z as we only computed B_ϕ for the $z=0$ plane. So we cannot directly check that this equation is valid.

Maxwell's Equations

We now have a complete system of equations for electromagnetism.

Sources

$\rho(\vec{r})$

$\vec{J}(\vec{r}, t)$

satisfy continuity equation

$$\vec{\nabla} \cdot \vec{J} = -\frac{\partial \rho}{\partial t}$$

Sources are described by source densities:

$$\rho(\vec{r}, t)$$

$$\vec{J}(\vec{r}, t)$$

Sources produce fields that satisfy Maxwell's equations

$$\vec{\nabla} \cdot \vec{E} = \frac{\rho(\vec{r}, t)}{\epsilon_0}$$

$$\vec{\nabla} \times \vec{E} = -\frac{\partial \vec{B}}{\partial t}$$

$$\vec{\nabla} \cdot \vec{B} = 0$$

$$\vec{\nabla} \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t}$$

Sources produce fields

\vec{E}

\vec{B}

Fields exert forces on test charges

$$\vec{F} = q(\vec{E} + \vec{v} \times \vec{B})$$

Lorentz force law

If sources are localized and fields $\rightarrow 0$ infinitely far away then these equations have unique solutions. Solve to get \vec{E}, \vec{B}